

TAILORING OF FLATTENED DISPERSION IN TRIANGULAR-LATTICE PHOTONIC CRYSTAL FIBER

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Abstract :

The interest of researchers and engineers in several laboratories, since the 1980s, has been attracted by the ability to structure materials on the scale of the optical wavelength, a fraction of micrometers or less, in order to develop new optical medium, known as photonic crystals. Photonic crystals rely on a regular morphological microstructure of air-holes, incorporated into the material, which radically alters its optical properties. In Photonic Crystal Fiber (PCF) it is possible to realize flat dispersion over a wide wavelength range that cannot be realized with a conventional single-mode fiber. In PCFs, the dispersion can be controlled and tailored with unprecedented freedom. In fact, due to the high refractive index difference between silica and air, and to the flexibility of changing air-hole sizes and patterns, the waveguide contribution to the dispersion parameter can be significantly changed, thus obtaining unusual position of the zero dispersion wavelength, as well as particular values of the dispersion curve slope. In particular, by manipulating the air-hole radius or the lattice period of the micro structured cladding, it is possible to control the zero-dispersion wavelength, which can be tuned over a very wide range, or the dispersion curves, which can be engineered to be ultra flattened. In this paper the geometric parameters of triangular PCF have been properly changed to optimize the dispersion compensation over a wide wavelength range.

Keywords: Photonic crystal fiber (PCFs), Dispersion compensating fiber (DCF), Single mode fiber (SMFs), Wavelength division multiplexing (WDM), Dispersion (D)

I. Introduction

Due to the flexibility for the cross section design, photonic crystal fibers (PCFs) have achieved excellent properties in dispersion [1-10], single polarization single mode [11-13], nonlinearity [14], and effective mode area [15-17], and also excellent performances in the applications of fiber sensors [18-19], fiber lasers [20-22] and nonlinear optics [23-26] over the past several years. Large numbers of research papers have highlighted some optical properties of the PCFs such as ultrahigh birefringence and unique chromatic dispersion, which are almost impossible for the conventional optical fibers.

The tendency for different light wavelengths to travel at different speeds is a crucial factor in the telecommunication system design. A sequence of short light pulses carries the digitized information. Each of these is formed from a spread of wavelengths and, as a result of chromatic dispersion, it broadens as it travels, thus obscuring the signal. The magnitude of the dispersion

changes with the wavelength, passing through zero at 1.3 μm in conventional optical fibers. For example, as the air-holes get larger, the PCF core becomes more and more isolated, until it resembles an isolated strand of silica glass suspended by six thin webs of glass. If the whole structure is made very small, the zero-dispersion wavelength can be shifted to the visible light, since the group velocity dispersion is radically affected by pure waveguide dispersion. On the contrary, very flat dispersion curves can be obtained in certain wavelength ranges in PCFs with small air-holes, that is with low air-filling fraction. First of all, the study of the dispersion properties of triangular PCFs with a high air-filling fraction, that is with small hole-to-hole spacing and large air-holes, is designed to compensate the anomalous dispersion and the dispersion slope of single-mode fibers [27–29]. In particular, the geometric parameters which characterize these triangular PCFs have been chosen to optimize the fiber length and the dispersion compensation over a wide wavelength range.

II. Dispersion compensation in triangular lattice PCFs

PCFs with a high air-filling fraction have been designed in order to compensate the anomalous dispersion and the dispersion slope of SMFs. In fact, their chromatic dispersion limits the data transmission rate in broadband wavelength division multiplexing (WDM) systems. In particular, it becomes a critical issue as soon as the transmission bit-rate increases over 10 Gb/s. The positive dispersion of installed fibers can be compensated by dispersion compensating fibers (DCFs) with a large dispersion of opposite sign. For WDM systems this goal must be achieved over a broad wavelength range around 1550 nm, thus implying, besides large negative dispersion values, a proper negative dispersion slope. The present analysis has demonstrated that PCFs can be exploited to this aim. In fact, their dispersion properties can be modified with high flexibility, since the large refractive index variation between silica and air permits to achieve significant waveguide dispersion over a wide wavelength range. PCFs with large air-holes have been already proposed for dispersion compensation, even though their description has been performed through a simplified model consisting of a silica core in air [30]. When the wavelength increases, this approximation gets worse.

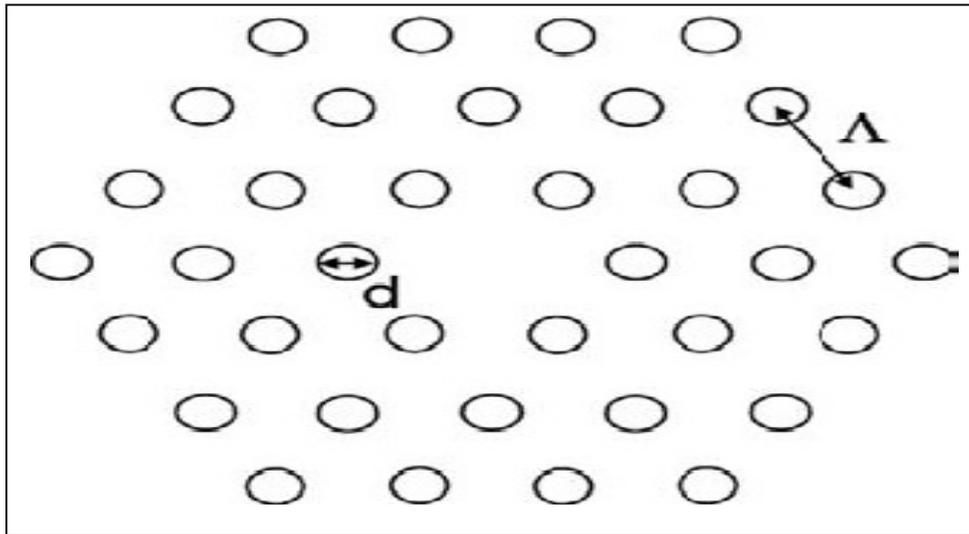


Fig. 1: Cross-section of a triangular PCF with the air-hole diameter d and the pitch Λ .

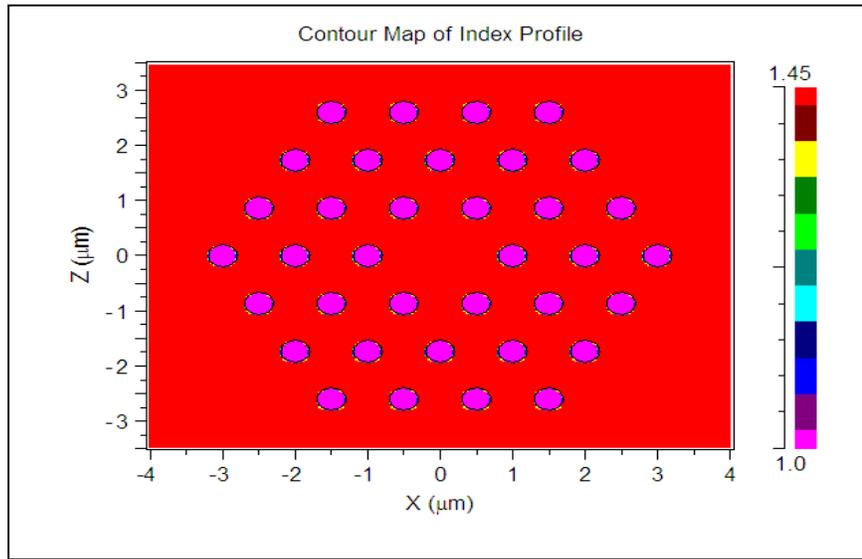


Fig.2 : Index profile of the triangular lattice PCF structure

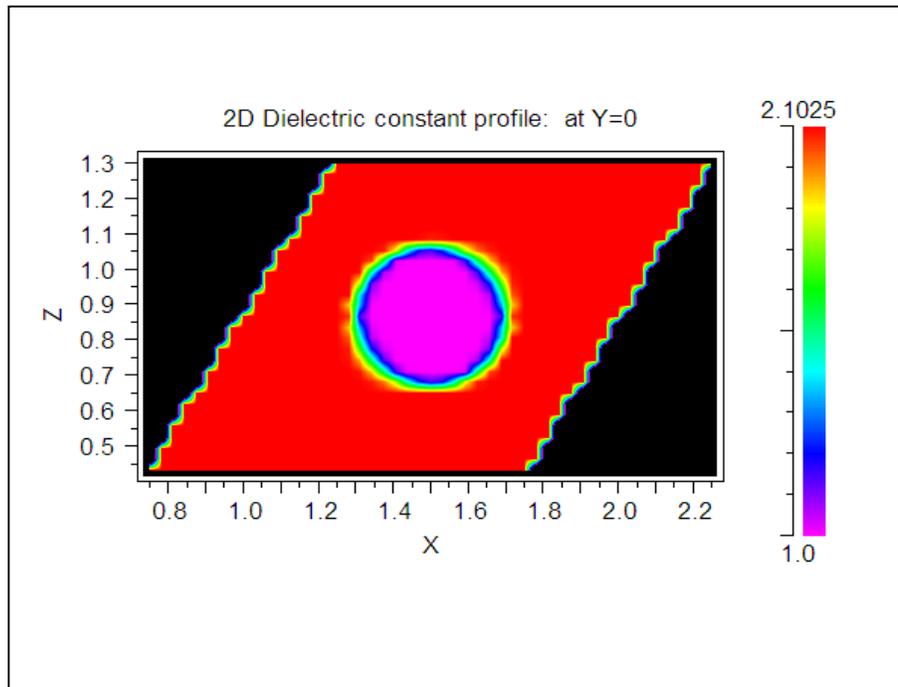


Fig.3 : Mode view of the triangular lattice PCF structure

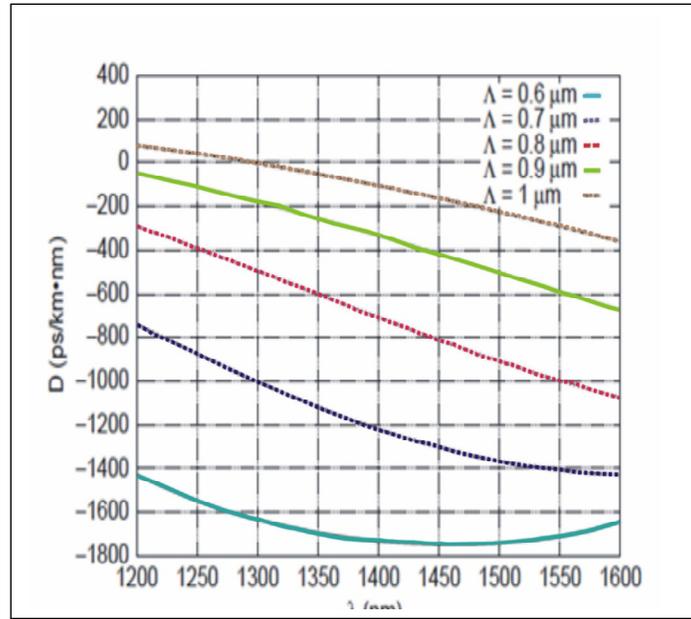


Fig. 4: Dispersion parameter for PCFs with $d/\Lambda = 0.9 \mu\text{m}$ and different Λ values

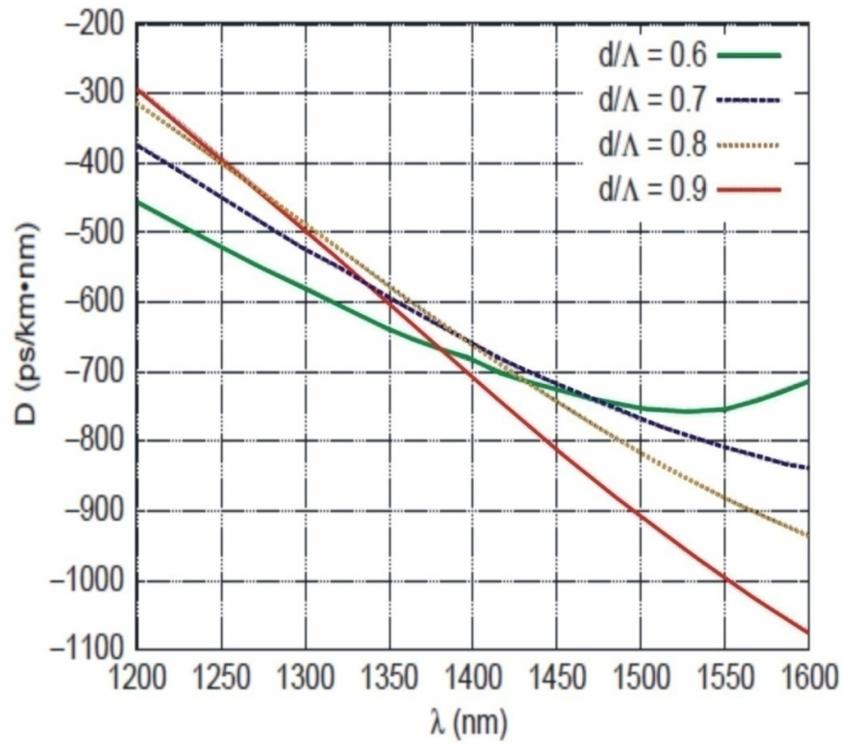


Fig. 5: Dispersion parameter for PCFs with $\Lambda = 0.8 \mu\text{m}$ and different d/Λ values

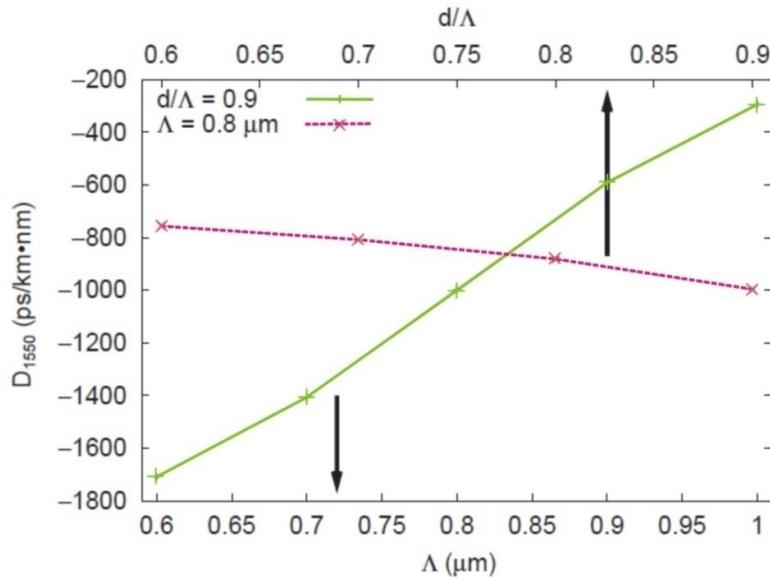


Fig. 6: Chromatic dispersion value at 1550 nm for the different triangular PCFs considered

III. Results and Discussion

In this study, the design of triangular PCFs has been optimized by properly tailoring the air-hole diameter d and the pitch Λ , as shown in Fig. 1, in order to compensate both the positive dispersion and the positive dispersion slope of single-mode fibers over a wavelength range around 1550 nm. To this aim, triangular PCFs with large air-holes and a small pitch, that is with a small core diameter $d_{\text{core}} = 2\Lambda - d = \Lambda \cdot (2 - d/\Lambda)$, have been considered. For the triangular PCFs here studied, a proper number of air-hole rings has been considered in order for the solution to converge toward that of a fiber with an infinite photonic crystal cladding. This results in a considerable reduction of the leakage losses [31]. In this paper the radiation field is evaluated by using FEM formulation. It has been shown that, by choosing the ring number between three and ten, leakage losses of fibers with d/Λ in the range 0.6–0.9 can be reduced under the Rayleigh scattering limit [32,33]. The dispersion parameter D has been derived in the wavelength range 1200 nm–1600 nm. The first fibers considered have $d/\Lambda = 0.9$ and Λ which varies between 0.6 and 1 μm . Fig. 4 shows their dispersion parameter D for the wavelengths between 1200 and 1600 nm. D is always negative if $\Lambda < 1 \mu\text{m}$ and becomes positive only for the triangular PCF with $\Lambda = 1 \mu\text{m}$ when $\lambda < 1300 \text{ nm}$. The absolute value of the dispersion parameter increases reducing the hole to hole spacing Λ . For the triangular PCF with $\Lambda = 0.6 \mu\text{m}$ D reaches a value around $-1700 \text{ ps/km} \cdot \text{nm}$ at 1550 nm, while for conventional DCFs it is typically $-100 \text{ ps/km} \cdot \text{nm}$ at this wavelength [30,36]. The dispersion slope is always negative in the wavelength range considered if $\Lambda \geq 0.7 \mu\text{m}$, while for the PCF with the smallest pitch, $\Lambda = 0.6 \mu\text{m}$, D reaches a minimum at 1475 nm and then the dispersion slope becomes positive. In order to optimize the PCF design, the effect of d variation has been investigated. For this reason the pitch has been fixed to $\Lambda = 0.8 \mu\text{m}$, that is, a middle value between those previously considered, and the ratio d/Λ has been varied from 0.9 to 0.6. As shown in Fig. 5, D is always negative in the wavelength range chosen for all the d/Λ values. As d/Λ decreases from the initial value of 0.9, the dispersion slope changes and becomes positive for the PCF with $d/\Lambda = 0.6$ if $\lambda > 1525 \text{ nm}$. The minimum value of D at 1550 nm, around $-1000 \text{ ps/km} \cdot \text{nm}$, has been obtained with the largest air-holes, that is, with $d/\Lambda = 0.9$. Results are summarized in Fig. 6, which shows the dispersion parameter values at 1550 nm. Notice that the dispersion value increases

significantly with Λ when d/Λ is fixed to 0.9, while it slowly decreases when the air-holes become larger, as in the case $\Lambda = 0.8 \mu\text{m}$. This result suggests important technological considerations. In fact, proper pitch values, rather than high air-filling fractions, allow to get fibers with dispersion values slightly affected by small variations of the air-hole diameter, eventually introduced by the fabrication process.

The anomalous dispersion of an SMF at 1550 nm is completely compensated by a DCF if

$$D_{\text{SMF}} \cdot L_{\text{SMF}} + D_{\text{DCF}} \cdot L_{\text{DCF}} = 0,$$

where D_{SMF} , D_{DCF} , L_{SMF} , and L_{DCF} are, respectively, the dispersion parameters and the lengths of the single-mode and the dispersion-compensating fibers. For a given SMF, if the absolute value of D_{DCF} is bigger, the length of the DCF can be shorter. The triangular PCF with $\Lambda = 0.6 \mu\text{m}$ and $d/\Lambda = 0.9$, which has the largest value of negative dispersion at 1550 nm, as shown in Fig.4, can be about 17 times shorter than a classical DCF. Unfortunately this fiber has a positive dispersion curve slope in the third window. In fact, the dispersion slope is very important, being the parameter which characterizes the dispersion compensation over a wavelength range. In an SMF the slope of $D(\lambda)$ at 1550 nm is positive. The two PCFs, with $\Lambda = 0.6 \mu\text{m}$ and $d/\Lambda = 0.9$ in Fig. 4 and with $\Lambda = 0.8 \mu\text{m}$ and $d/\Lambda = 0.6$ in Fig. 5, have a positive dispersion slope too, so they are suitable for dispersion compensation only at one wavelength. In particular, the latter PCF has a lower value of D at 1550 nm, -755 ps/km nm . All the other PCFs present a negative dispersion slope at 1550 nm and can be exploited to compensate the anomalous dispersion of an SMF over a wide wavelength range.

IV CONCLUSIONS

The analysis performed above have shown that, by properly changing the geometric characteristics of the air-holes in the PCF cross-section, the waveguide contribution to the dispersion parameter can be significantly changed, thus obtaining unusual positions of the zero-dispersion wavelength, as well as particular values of the dispersion curve slope. By manipulating the air-hole radius or the lattice period of the micro structured cladding, it is possible to control the zero-dispersion at wavelength around 1550 nm, which can be tuned over a very wide wavelength range, and the dispersion curves can be engineered to be ultra flattened. The PCFs with these characteristics and with a small effective area, that is a high nonlinear coefficient are suitable for a great number of telecommunication applications, such as wavelength conversion or optical parametric amplification. It is believed that the analysed PCF will have promising future in ultra broadband transmission applications.

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